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Abstract

Isothermal CFD analysis was performed on axially opposed rows of jets mixing with crossflow in a rectangular duct. Laterally, the jets' centerlines were aligned with each other on the top and bottom walls. The focus of this study was to characterize the effects of orifice aspect ratio and jet-to-mainstream mass flow ratio on jet penetration and mixing. Orifice aspect ratios (L/W) of 4-to-1, 2-to-1, and 1-to-1, along with circular holes, were parametrically analyzed. Likewise, jet-to-mainstream mass flow ratios (MR) of 2.0, 0.5, and 0.25 were systematically investigated. The jet-to-mainstream momentum-flux ratio (J) was maintained at 36 for all cases, and the orifice spacing-to-duct height (S/H) was varied until optimum mixing was attained for each configuration.

The numerical results showed that orifice aspect ratio (and likewise orifice blockage) had little effect on jet penetration and mixing. Based on mixing characteristics alone, the 4-to-1 slot was comparable to the circular orifice. The 4-to-1 slot has a smaller jet wake which may be advantageous for reducing emissions. However, the axial length of a 4-to-1 slot may be prohibitively long for practical application,

especially for MR of 2.0. The jet-to-mainstream mass flow ratio had a more significant effect on jet penetration and mixing. For a 4-to-1 aspect ratio orifice, the design correlating parameter for optimum mixing [$C = (S/H)\sqrt{J}$] varied from 2.25 for a mass flow ratio of 2.0 to 1.5 for a mass flow ratio of 0.25.

Nomenclature

C	$(S/H)\sqrt{J}$ (see Eq. 1)
C_{avg}	$m_j / (m_j + m_\infty) = \theta_{EB}$
H	Duct Height
J	Momentum-Flux Ratio $(\rho_j V_j^2) / (\rho_\infty U_\infty^2)$
L	Orifice Length (long dimension)
L/W	Orifice Aspect Ratio (SAR in previous reports)
m_j	Mass Flow of Jets
m_∞	Mass Flow of Mainstream
MR	Mass Flow Ratio m_j / m_∞
P	Pressure (N/m^2)
S	Orifice Spacing
S/H	Orifice Spacing-to-Duct Height Ratio
T	Temperature (K)
U_∞	Mainstream Flow Velocity (m/s)
U	Unmixedness (see Eq. 2)
u	rms of Axial Velocity Fluctuation

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v	rms of Vertical Velocity Fluctuation
W	Orifice Width (short dimension)
x	Axial Coordinate, $x=0$ at leading edge of the orifice
x/H	Axial Distance-to-Duct Height Ratio
V_j	Jet Velocity (m/s)
y	Vertical Coordinate
z	Lateral Coordinate
μ_T	Turbulent Viscosity (kg/m-sec)
ρ_j	Density of Jet
ρ_∞	Density of Mainstream

1. Introduction

In recent years increased public awareness on issues such as global warming and upper atmosphere ozone depletion have sparked a growing concern over the environment. Despite the ever tightening emissions regulations, the vast majority of upper atmosphere pollutants still originate from combustion systems. To meet the increasing stringent air quality standards, low emission combustors must be developed.

One such concept being evaluated both experimentally and numerically is the Rich-burn/Quick-mix/Lean-burn (RQL) combustor¹. This combustor utilizes staged burning in which the primary zone is designed to operate fuel rich at equivalence ratios exceeding one.² The combustion products high in carbon monoxide concentration enter the quick-mix section where mixing is initiated with bypass air. The combustion process is then completed in the lean-burn region.

In order to make the RQL combustor a viable combustor concept for low emissions, rapid and uniform mixing must take place in the quick-mix section. Recent studies have been performed that focus on identifying improved mixing concepts.³⁻¹⁷

2. Background

The mixing of jets in a confined crossflow has proven to have far reaching practical applications and has

spurred a variety of research studies over the last quarter of a century. In gas turbine combustors, jet mixing is particularly important in the combustor dilution zone. The dilution zone is the aft zone where the products of combustion are mixed with air to produce a temperature profile acceptable to the turbine.¹⁸⁻²⁰

Dilution zone mixing studies¹⁸ have identified two significant design parameters that influence the mixing pattern: 1) jet-to-mainstream momentum-flux ratio (J) and 2) orifice spacing-to-duct height ratio (S/H). Optimum mixing relationships were determined to be a function of the product of S/H and square root of J for the range of conditions tested and analyzed:

$$C = (S/H)\sqrt{J} \quad (1)$$

One-sided injection (from the top wall only) and two-sided injection (from both the top and bottom walls) were studied. The optimum mixing constants were identified as shown in Table 1. For two-sided, axially opposed rows of jets with jets' centerlines aligned, optimum mixing was obtained when C was 1.25. The best mixing occurred when the dilution jets penetrated to about one-quarter duct height.

In contrast to conventional dilution zones, the quick-mix section of RQL combustors has a larger jet-to-mainstream mass flow ratio ($MR \geq 2.0$ vs. ≤ 0.5). Such a large MR for RQL combustors might necessitate the use of slots rather than holes in the combustor liner. It is unclear whether orifice aspect ratio affects jet mixing, especially at large mass flow ratios. It is also unclear if design correlations developed for $MR < 0.5$ are applicable to large $MR (\geq 2.0)$. This study sought to address these issues by a systematic computational investigation. A complete description of the cases studied and their results are discussed below.

3. CFD Code

The approach in this study was to perform 3-D numerical calculations on a generic geometry section.

The CFD code named CFD-ACE²¹ was used to perform the computations. The basic capabilities/methodologies in CFD-ACE include:

- (1) co-located, fully implicit and strongly conservative finite volume formulation;
- (2) solution of two- and three-dimensional Navier-Stokes equations for incompressible and compressible flows;
- (3) non-orthogonal curvilinear coordinates;
- (4) multi-domain grid topology;
- (5) upwind, central (with damping), second order upwind and Osher-Chakravarthy differencing schemes;
- (6) standard²², extended²³, and low Reynolds number²⁴ K- ϵ turbulence models;
- (7) instantaneous, one-step, and two-step heat release and emission combustion models;
- (8) spray models including trajectory, vaporization, etc.; and
- (9) pressure-based solution algorithms including SIMPLE and a variant of SIMPLEC.

4. Details of Numerical Calculations

A schematic of the computational model is shown in Figure 1. The height of the mixing section was 4 inches (0.1016 m). The mainstream flow entered the calculation domain one duct height upstream (x/H of -1.0) of the leading edge of the orifices, and continued downstream to x/H of 7.0. The model consisted of jet injection from top and bottom walls into mainstream flow. Three slot orifices were analyzed, having aspect ratios of 4-to-1, 2-to-1, and 1-to-1. A circular orifice was also analyzed for completeness. The slots were aligned with the long dimension in the direction of the mainstream flow.

The rows of orifices located on the top and bottom walls were in the same axial plane and inline in the lateral direction. The lateral calculation domain extended from midplane to midplane between the jets'

centerlines. Periodic boundary conditions were imposed on the lateral boundaries.

Six parametrics consisting of 31 cases were analyzed as shown in Table 2. The case sequence for each parametric consisted of holding J , MR , and L/W constant, and then parametrically changing S/H to optimize mixing. As S/H was varied, the slot dimensions changed to maintain a constant jet-to-mainstream mass flow ratio. For each parametric, the slot geometry producing optimum mixedness is shown in Figure 2. Parametrics 1, 2, and 3 show the effect of MR . A 4-to-1 slot orifice was held constant in parametrics 1, 2, and 3. Parametrics 1, 4, 5, and 6 show the effect of orifice aspect ratio. The mass flow ratio was held constant at 2.0 for parametrics 1, 4, 5, and 6.

The flow conditions of the mainstream and jets were

<u>Mainstream</u>	<u>Jets</u>
$U_{\infty} = 10 \text{ m/s}$	$V_j = 60 \text{ m/s}$
$T_{\infty} = 300 \text{ K}$	$T_j = 300 \text{ K}$
$u/U_{\infty} = 0.20$	$v/V_j = 0.20$
$\mu_T = 1 \times 10^{-2}$	$\mu_T = 1 \times 10^{-2}$
$\text{kg/m}\cdot\text{sec}$	$\text{kg/m}\cdot\text{sec}$
$P = 1 \times 10^5 \text{ N/m}^2$	
$J = 36$	
$m_j/m_{\infty} = 2.0, 0.50, 0.25$	

The turbulent length scales of the jets were varied to maintain a constant inlet turbulent viscosity.

Grids

A typical case consisted of 60,000 cells, 64 cells in the axial (x) direction, 28 cells in the vertical (y) direction, and 34 cells in the lateral (z) direction. The slots were composed of uniformly distributed cells; 192 cells (24×8) for the 4:1 slot, 384 cells (24×16) for the 2:1 slot, and 528 cells (24×24) for the 1:1 slot. The circle was generated using boundary fitted coordinates and was

composed of 576 cells. The grid upstream and downstream of the orifice region was expanded/contracted so that each cell adjacent to the slot region matched the cell size in the slot region. The cells in the vertical direction were all of uniform size.

Numerics

The following conservation equations were solved: u momentum, v momentum, w momentum, mass (pressure correction), turbulent kinetic energy (k), and turbulent energy dissipation (ϵ). The convective fluxes were calculated using upwind differencing, and the diffusive fluxes were calculated using central differencing. The standard k- ϵ turbulence model was employed and conventional wall functions were used.

Convergence

All error residuals were reduced at least 6 orders of magnitude, and continuity was conserved in each axial plane to the fifth decimal. Convergence was relatively smooth requiring about 600 iterations. A converged solution required approximately 4.0 CPU hours on a CRAY-YMP computer.

5. Data Postprocessing

Graphics postprocessing was performed using NASA PLOT3D software.²⁵ The only exception was Figure 11 which was processed using CFD-VIEW.^{26,27}

In order to quantify the mixing effectiveness, the mass-averaged spatial concentration variance of jet flow (C_{var}) was calculated in each axial plane. The mass-averaged unmixedness (U) is defined²⁸ as

$$U = C_{var} / [C_{avg} (1 - C_{avg})] \quad (2)$$

where

$$\begin{aligned} C_{var} &= (1/m_{TOT}) \sum_i m_i (C_i - C_{avg})^2 \\ m_{TOT} &= \text{total mass flow in each axial plane} \\ m_i &= \text{mass flow of cell } i \\ C_i &= \text{jet mass fraction in cell } i \end{aligned}$$

$$C_{avg} = m_j / (m_j + m_\infty) = \theta_{EB}^{17} \quad (\text{downstream of orifice})$$

Calculating the unmixedness parameter can be broken down into two parts: 1) in the orifice (jet injection) region, and 2) aft of the trailing edge of the orifice. Downstream of the orifice all of the jet flow has been added and C_{avg} is a constant value as defined above. In the orifice region, C_{avg} is calculated in each axial plane based on the amount of jet mass in that plane. The unmixedness curves show a sharp spike (just downstream of x/H of 0) where the jet flow first enters the domain and then gradually drops as the jet flow begins to mix with the mainstream flow.

6. Results and Discussion

Figure 3 presents the unmixedness results for all of the parametrics. The optimum mixing curve for each parametric is illustrated by the bold line. Note that the inflection points in the unmixedness curves identify the location of the trailing edge of the orifice. Discussion of the results follows.

Effect of Jet-to-Mainstream Mass Flow Ratio

The effect of MR on jet penetration is presented in Figure 4. Plotted are the jet mass fraction color concentrations in a lateral plane through the orifice centerline. S/H is held constant (0.275) in the figure. The color bar distribution was the same for all three MR cases in Figure 4. Each color bar has an arrow signifying the overall jet mass fraction at equilibrium. It is hard to discern differences in jet penetration with this color bar since mixed-out (equilibrium) values of mass fraction vary significantly between MR cases. An alternate way to compare jet penetration is to alter the color bar distribution such that the color at mixed-out conditions is maintained for each MR case. Figure 5 is similar to Figure 4 but with the revised color bar for each MR case.

For the MR of 2.0 case, the jets are somewhat underpenetrated, allowing too much of the approach

flow to pass through the center of the duct. In contrast, for MR of 0.25, the jets are somewhat overpenetrated as evidenced by more mainstream flow being forced between the jets. For MR of 0.50, the jets have penetrated to 1/4 duct height and an equal balance of mainstream flow has passed through the center of the duct and between the jets. Thus, a significant effect of MR on jet penetration is seen.

Figure 6 presents unmixedness results for each MR at the optimum S/H . Note that the optimum S/H is 0.375 for MR of 2.0, while the optimum S/H is 0.25 for MR of 0.25. Such a variation in optimum S/H shows there is significant effect of MR on unmixedness. In the orifice region, a large difference is seen between the different MR due to the large variation in orifice geometric size. Although the MR of 2.0 case exhibits the lowest value of unmixedness at the orifice leading edge, it has the highest value of unmixedness at x/H between 0.3 and 0.5 because of the slot's length. For $x/H > 0.7$, the MR of 2.0 case exhibits slightly better mixing than the other two MR cases.

Figure 7 presents the jet mass fraction contours in a lateral plane through the orifice centerline for each mass flow ratio. Figure 7 is similar to Figure 5 except the results are shown at optimum S/H instead of constant S/H . Figure 8 presents the jet mass fraction contours for each mass flow ratio in an axial plane (x/H of 0.5). Optimum S/H cases are shown. At this axial location, the jets for the MR of 2.0 case are still entering the flowfield. For the other two MR cases, it can be seen there is equal balance of mainstream flow in the center of the duct and along the ducts' walls.

Aspect Ratio Analysis

The effect of aspect ratio variation on jet penetration is seen in Figure 9. Note that all cases have MR of 2.0. Presented are jet mass fraction concentrations in a lateral plane taken through the orifice centerline. S/H was held constant (0.425) in the figure. For each aspect ratio case, the jets penetrate approximately one-quarter of the duct height. There are some subtle differences between

each aspect ratio case, the most recognizable being the difference between the square orifice (aspect ratio of 1-to-1) and the other orifices. The square orifice appears to penetrate slightly less than the other orifices as evidenced by less mainstream flow in the wakes of the jets (less green behind jets). However, in general, aspect ratio has little effect on jet penetration.

Figure 10 provides insight into why the square jet has slightly less penetration than the other orifices. Figure 10 presents the jet mass fraction concentrations in a vertical plane next to the top wall. Compared to the 4-to-1 and 2-to-1 slot orifices, the square orifice presents significantly more blockage to the mainstream flow. The blockage of the square orifice is 63% as compared to 44% and 31% for the 2-to-1 and 4-to-1 slot orifices. If the orifice aspect ratio is further decreased, the mainstream flow would be almost totally blocked from passing between jets. Thus, the slight decrease in jet penetration for the square orifice case is probably caused by jet blockage effects. It is interesting to note that the circle orifice, although having larger frontal area (and jet blockage, 71%), has less blockage effect on the mainstream flow than the square orifice. A possible cause of the reduced blockage effect of the circle is discussed in the next paragraph. It is interesting to note that Liscinsky¹⁵ has experimentally shown there is minimal effect of jet blockage for circle orifices having geometric blockages less than 75%.

The effect of slot aspect ratio on jet wakes is illustrated in Figure 11. Figure 11 presents velocity vectors in the vertical plane next to the top wall. Near the wall the jet acts like a bluff body to the mainstream flow. The mainstream flow accelerates around the jet before separating and forming a wake behind the jet. As the base area of the orifice increases, the size of the wake recirculation zone increases. Thus, the square orifice has a wake width approximately twice that of the 4-to-1 slot. The wake width of the circle orifice is less than the wake width of the square orifice because the mainstream flow stays attached around the circular jet before separating. Such flow attachment may be the

cause of slightly greater jet penetration of the circle compared to the square orifice. Wake sizes may have an impact on emissions in quick-mix strategies.

The effect on aspect ratio on unmixedness is illustrated in Figure 12. The unmixedness curves are presented at optimum S/H . In the orifice region there are sizable differences in the mixing between aspect ratios. The 4:1 slot had the best initial mixing followed by the 2:1, 1:1 and circle cases. Aft of the orifices' trailing edges, the different aspect ratio curves essentially yield the same level of unmixedness.

At x/H of 0.5, Figure 12 shows that the 4:1 slot is the most unmixed, while the 2:1 slot is the least unmixed, and the 1:1 slot and circle orifices are somewhere in between. Figure 13 gives insight into why the 4:1 slot is the most unmixed. Figure 13 shows the jet mass concentration contours of all four orifice shapes in an axial plane at x/H of 0.5. It can be seen that the 4:1 jets are still entering the flowfield at x/H of 0.5, resulting in a high degree of unmixedness. The most mixed appears to be the 2:1 slots and circle orifices.

Figure 14 shows a direct comparison of unmixedness for the 4-to-1 slot and circle cases. The optimum S/H for the slot is 0.375 while for the circle it is 0.425, almost the same. Aft of the slot trailing edge ($x/H > 0.5$), the mixing levels of both orifices are identical. In the orifice region, there are some differences between orifices. At the orifice leading edge, the slot has less unmixedness than the circle, but aft of the circle trailing edge and upstream of the slot trailing edge, the circle case has less unmixedness than the slot case. From an overall unmixedness viewpoint, the circle and slot appear to be similar.

Design Correlation Constant for Optimum Mixing

Shown in Table 3 is a comparison of the design correlation constants $[(S/H)\sqrt{J}]$ for optimum mixing. The constants are presented based on the numerical results of this study as well as based on previous experimental tests reported in the literature for low MR

(<0.5). For MR of 2.0, the numerically determined constant was significantly higher than for the MR of 0.25 case (2.25 vs. 1.50). The design constant based on previous experiments was 1.25 for MR less than 0.5. Thus, there appears to be a significant mass flow ratio effect.

The constants were determined to be 2.25 for the 4:1 and 2:1 cases and 2.55 for the 1:1 and circle cases. The design constant of 2.55 for circles is in agreement with recent isothermal experiments by Liscinsky.¹⁵ Thus, in an engineering sense, the design constants were nearly the same for the four different orifice configurations. This result is consistent with the unmixedness and jet penetration results signifying little effect of aspect ratio.

7. Conclusions

A CFD parametric mixing study was performed on axially opposed rows of inline jets injected into a confined rectangular crossflow. Design variables systematically investigated were orifice aspect ratio (4-to-1, 2-to-1, 1-to-1, and circle) and jet-to-mainstream mass flow ratio (2.0, 0.5, and 0.25). A constant jet-to-mainstream momentum-flux ratio (J) of 36 was maintained for all simulations. Based on the numerical analysis, the following conclusions can be drawn:

1. Slot aspect ratio had little effect on jet penetration and mixing.
2. Circle and slot orifices had similar mixing characteristics.
3. The jet wake recirculation zone increased in size as slot aspect ratio decreased, as expected.
4. Jet-to-mainstream mass flow ratio influenced jet penetration and mixing. The design correlation constant $[C = (S/H)\sqrt{J}]$ varied from 2.25 at a MR of 2.0 to 1.5 for a MR of 0.25. Previous experimental results had reported a design correlation constant of 1.25 for MR less than 0.5.

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Table 1. Spacing and Momentum-Flux Ratio Relationships

Configuration	$C = (S/H) \sqrt{(J)}$
Single-side injection:	
Under-penetration	<1.25
Optimum	2.5
Over-penetration	>5.0
Opposed rows of jets:	
In-line optimum	1.25
Staggered optimum	5.0

Table 2. Numerical Cases Analyzed

<u>Parametric</u>	<u>Case</u>	<u>Orifice Aspect Ratio</u>	<u>Momentum Flux Ratio</u>	<u>Mass Flow Ratio (m_j/m_m)</u>	<u>S/H</u>	<u>Trailing Edge X/H</u>	<u>Jet Blockage at Wall</u>
Parametric 1	Case 1	4:1	J=36	2.0	0.125	0.29	57.7
	Case 2	↓	↓	↓	0.20	0.36	45.6
	Case 3	↓	↓	↓	0.228	0.39	42.8
	Case 4	↓	↓	↓	0.25	0.41	40.8
	Case 5	↓	↓	↓	0.275	0.43	38.9
	Case 6	↓	↓	↓	0.325	0.47	35.8
	Case 7	↓	↓	↓	0.375*	0.50	33.3
	Case 8	↓	↓	↓	0.425	0.53	31.3
	Case 9	↓	↓	↓	0.50	0.58	28.9
	Case 10	↓	↓	↓	0.75	0.71	23.6
	Case 11	↓	↓	↓	1.0	0.82	20.4
Parametric 2	Case 12	4:1	J=36	0.50	0.125	0.14	28.9
	Case 13	↓	↓	↓	0.20	0.18	22.8
	Case 14	↓	↓	↓	0.250	0.20	20.4
	Case 15	↓	↓	↓	0.275*	0.21	19.5
	Case 16	↓	↓	↓	0.325	0.23	17.9
Parametric 3	Case 17	4:1	J=36	0.25	0.20	0.13	16.1
	Case 18	↓	↓	↓	0.25*	0.14	14.4
	Case 19	↓	↓	↓	0.275	0.15	13.8
Parametric 4	Case 20	2:1	J=36	2.0	0.30	0.32	52.7
	Case 21	↓	↓	↓	0.375*	0.35	47.1
	Case 22	↓	↓	↓	0.425	0.38	44.3
	Case 23	↓	↓	↓	0.45	0.39	43.0
	Case 24	↓	↓	↓	0.50	0.41	40.8
Parametric 5	Case 25	1:1	J=36	2.0	0.325	0.23	71.6
	Case 26	↓	↓	↓	0.375	0.25	66.7
	Case 27	↓	↓	↓	0.425*	0.27	62.6
	Case 28	↓	↓	↓	0.50	0.29	57.7
Parametric 6	Case 29	Circle-BFC	J=36	2.0	0.375	0.28	75.2
	Case 30	↓	↓	↓	0.425*	0.30	70.7
	Case 31	↓	↓	↓	0.50	0.33	65.1

* represents Optimum Mixing Configuration

Table 3. Experimentally¹⁸ and Numerically Determined Constants at Optimum S/H

Geometry	Lateral Arrangement	m_j/m_∞	Aspect Ratio	J	S/H	$C = (S/H)\sqrt{J}$	
						Experimental	Numerical
Two-Sided ↓	Inline ↓	2.0	4:1	36	0.375	1.25	2.25
		0.5	↓	↓	0.275	↓	1.65
		0.25	↓	↓	0.25	↓	1.50
		2.0	2:1	↓	0.375	↓	2.25
		↓	1:1	↓	0.425	↓	2.55
		↓	Circle	↓	0.425	↓	2.55

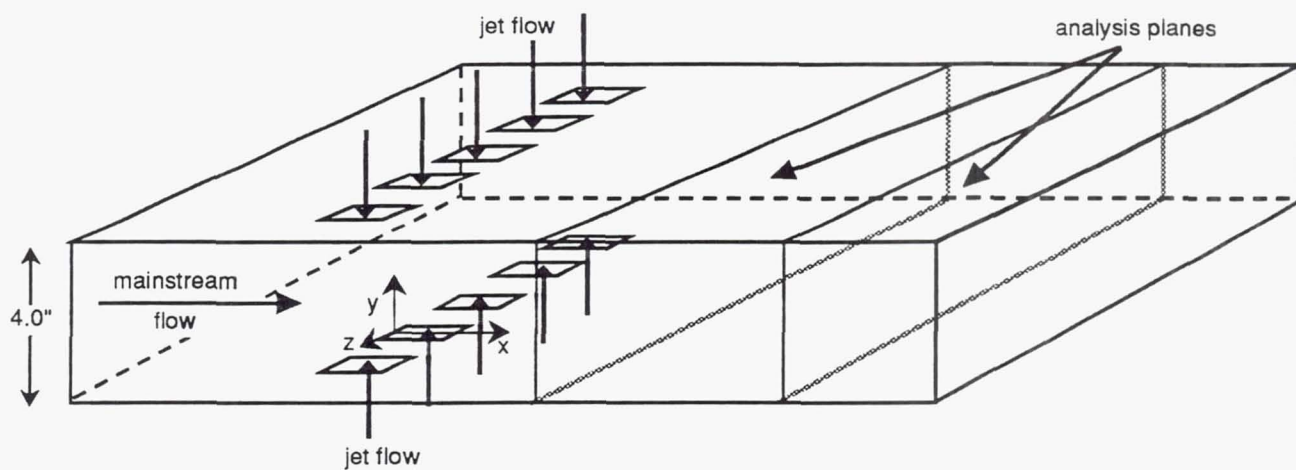


Figure 1. Schematic of Numerical Mixing Model

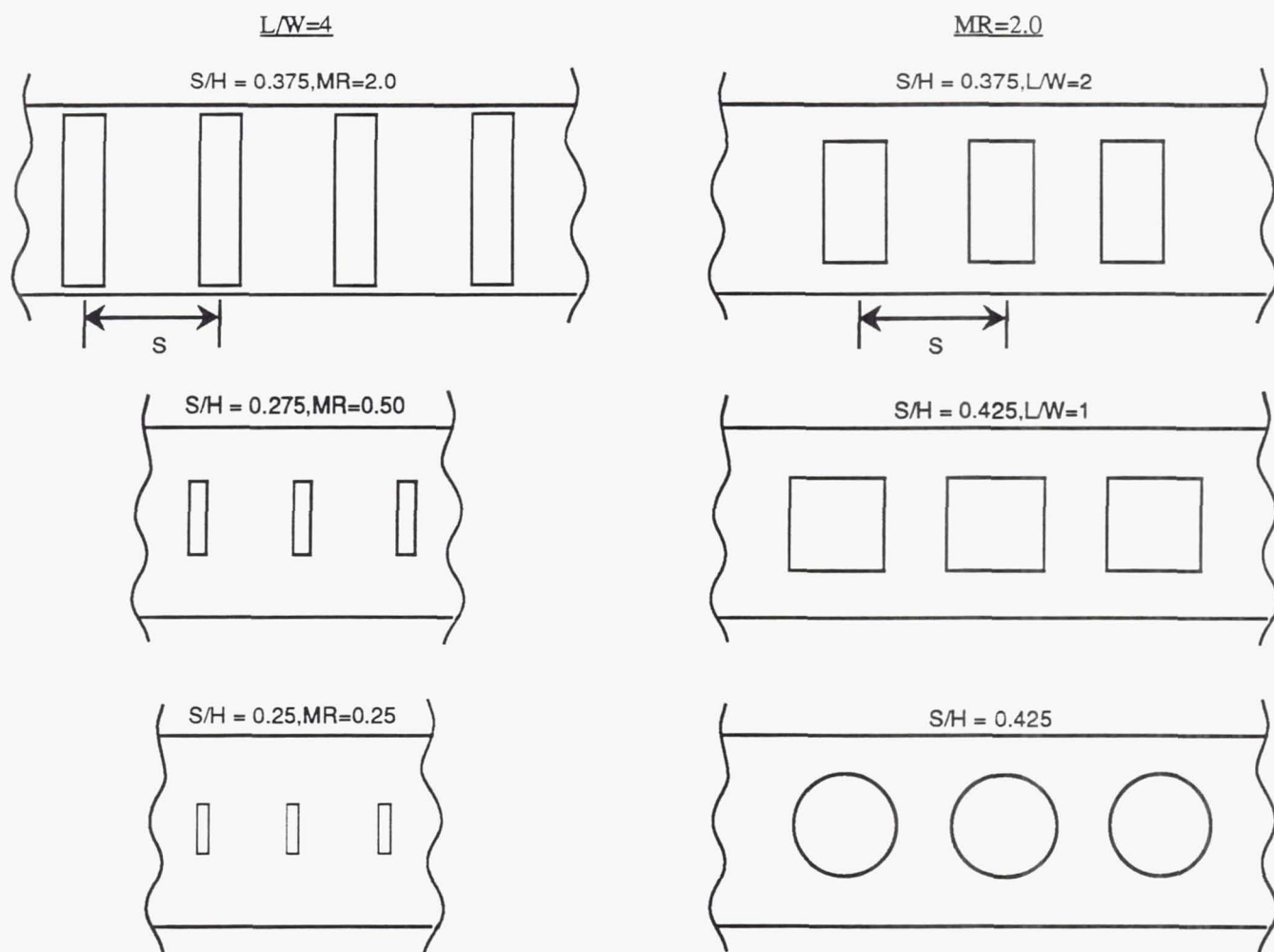


Figure 2. Slot Configurations At Optimum S/H

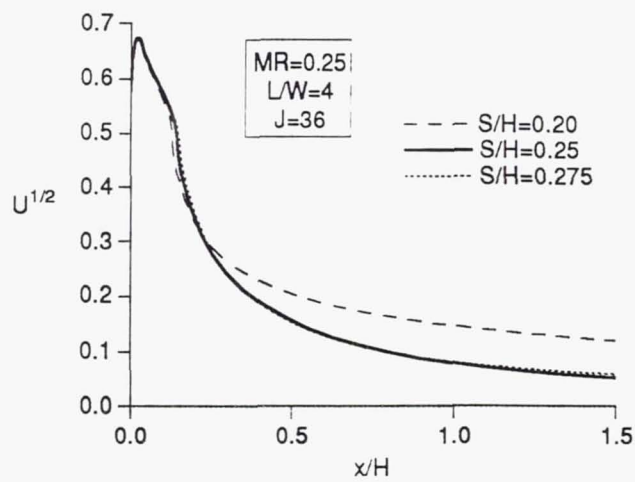
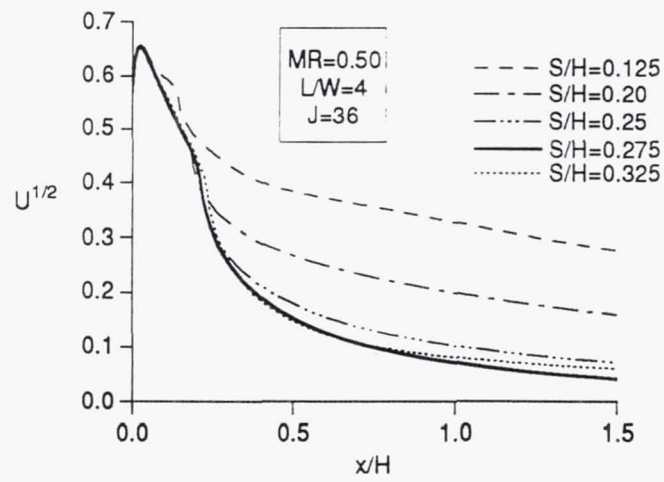
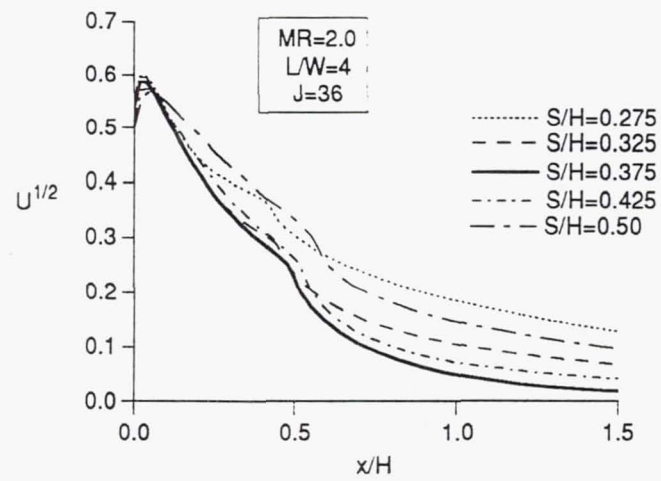


Figure 3. Computational Results of Parametrics 1-3

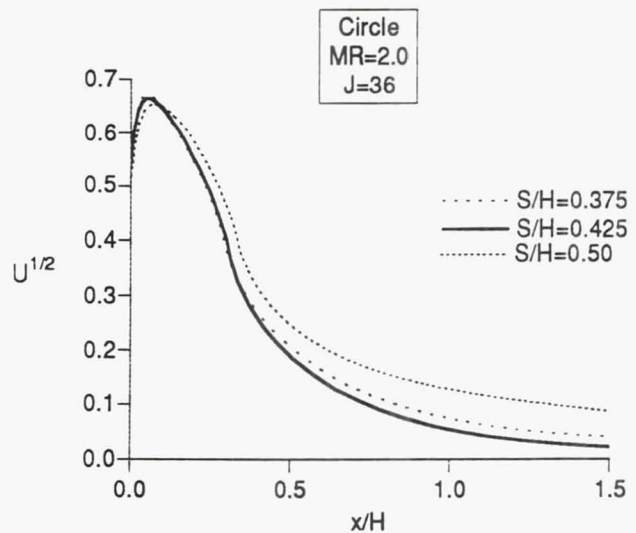
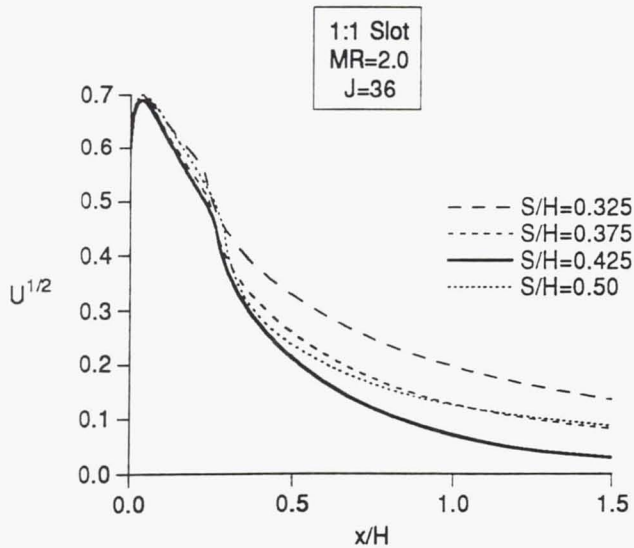
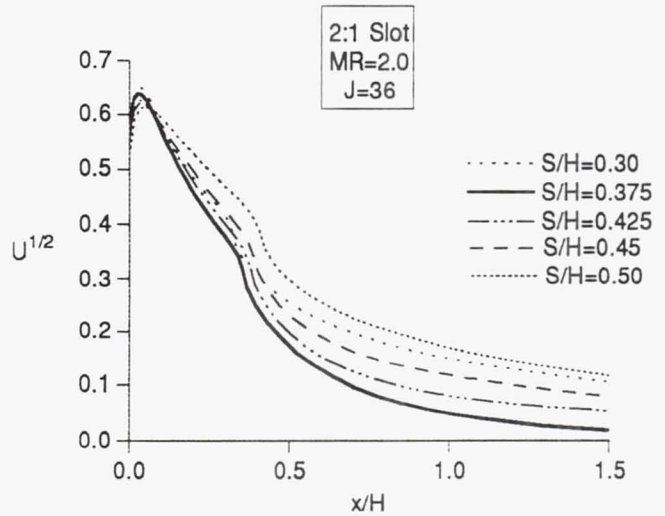
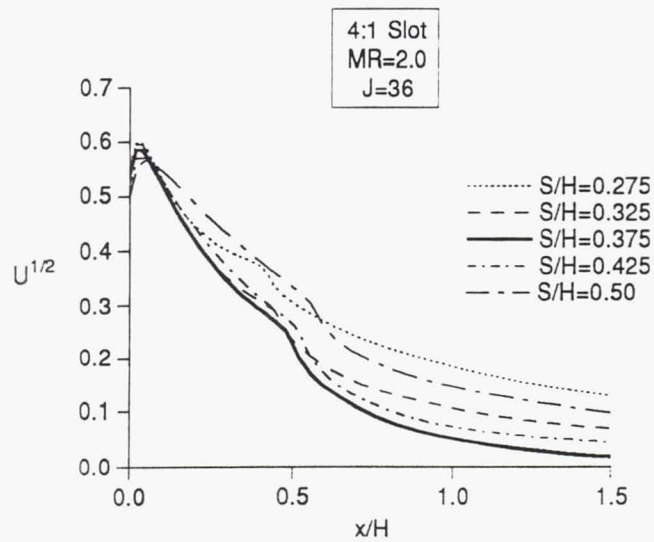


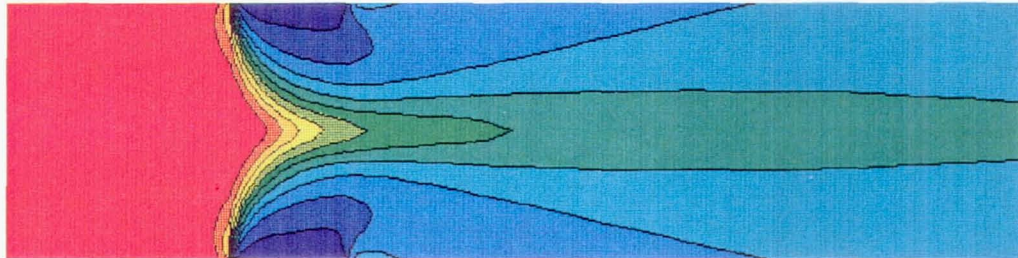
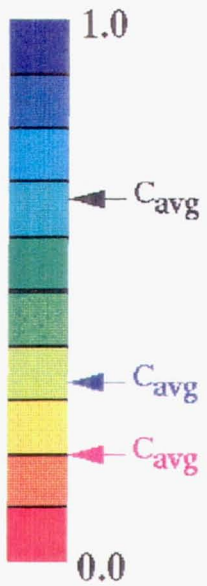
Figure 3. Computational Results of Parametrics 1, 4, 5, and 6 (cont'd)

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Slot Centerline @S/H=0.275

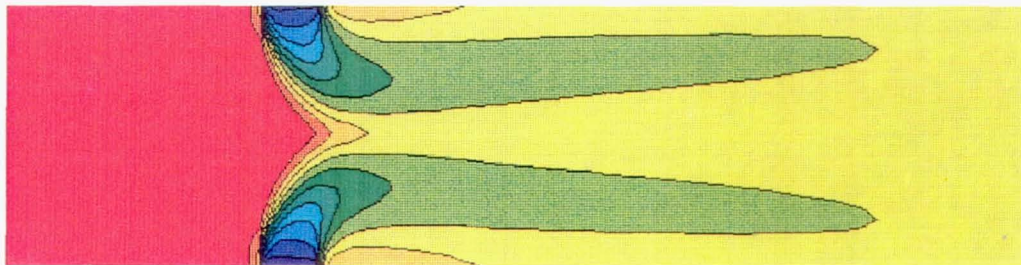
MR

Jet
Mass
Fraction



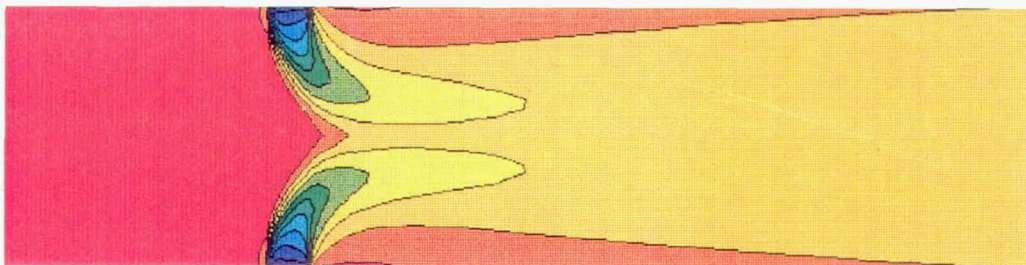
2.0

$C_{avg}=0.66$



0.50

$C_{avg}=0.33$



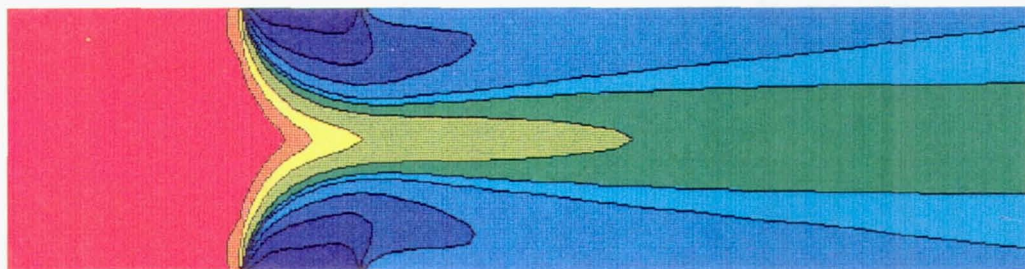
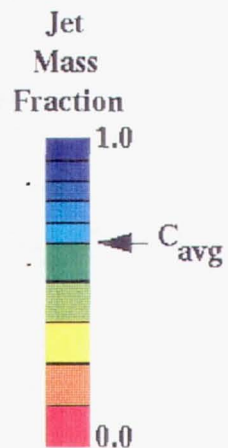
0.25

$C_{avg}=0.20$

Figure 4. Effect of Jet-to-Mainstream Mass Flow Variation on Jet Penetration: $J=36$, $L/W=4$ (Uniform Color Bar Distribution)

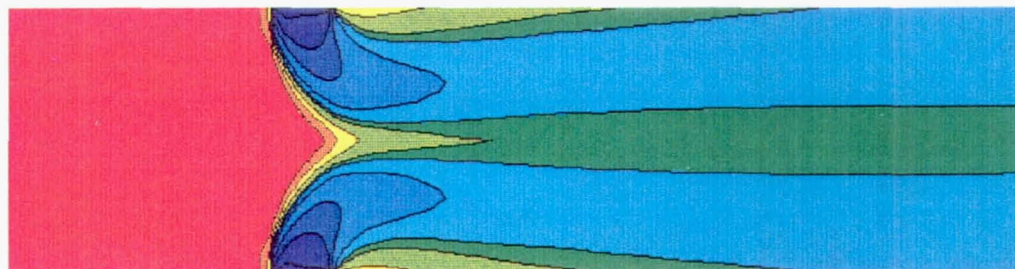
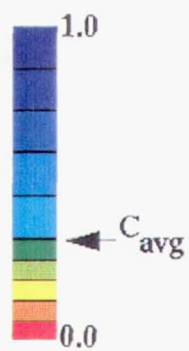
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Slot Centerline @S/H=0.275

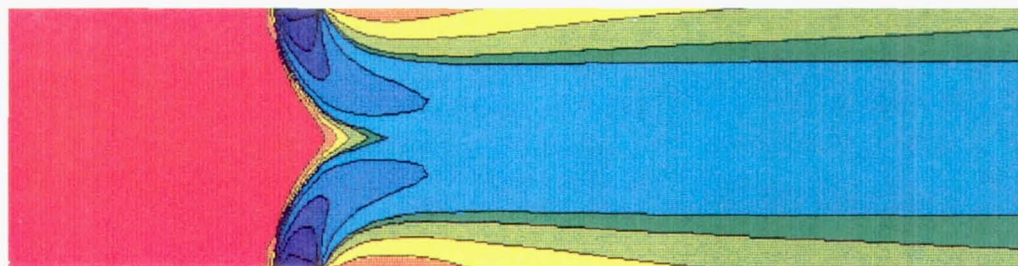
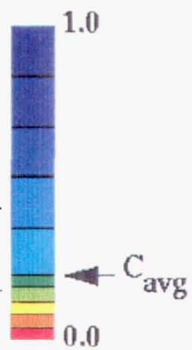


MR

2.0



0.50



0.25

Figure 5. Effect of Jet-to-Mainstream Mass Flow Variation on Jet Penetration: $J=36$, $L/W=4$ (Non-uniform Color Bar Distribution)

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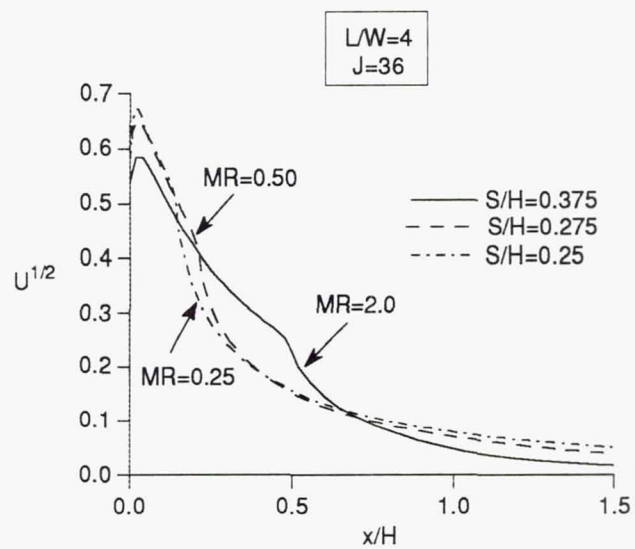
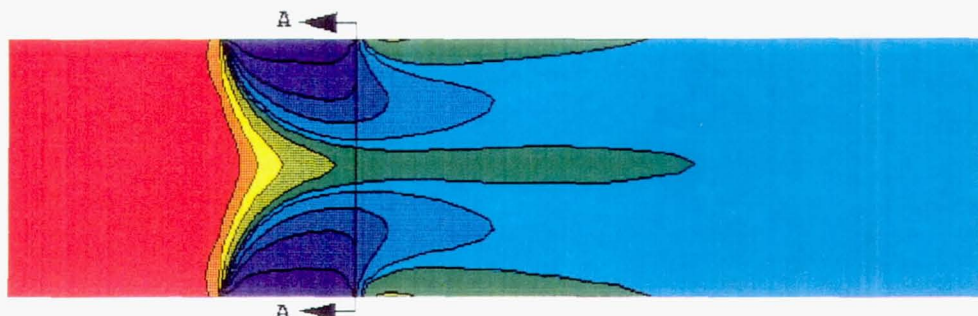
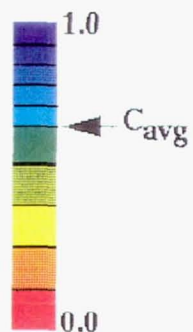


Figure 6. Effect of Jet-to-Mainstream Mass Flow Ratio on Unmixedness at Optimum S/H

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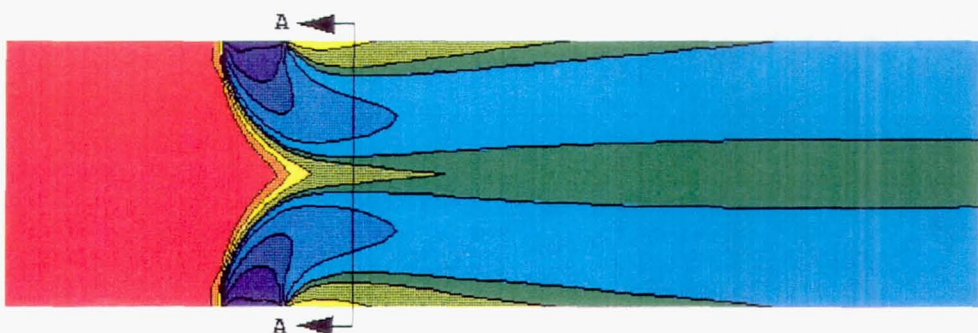
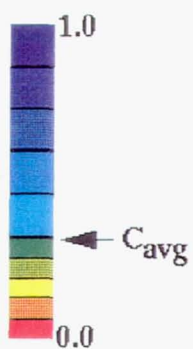
Slot Centerline @Optimum S/H

MR



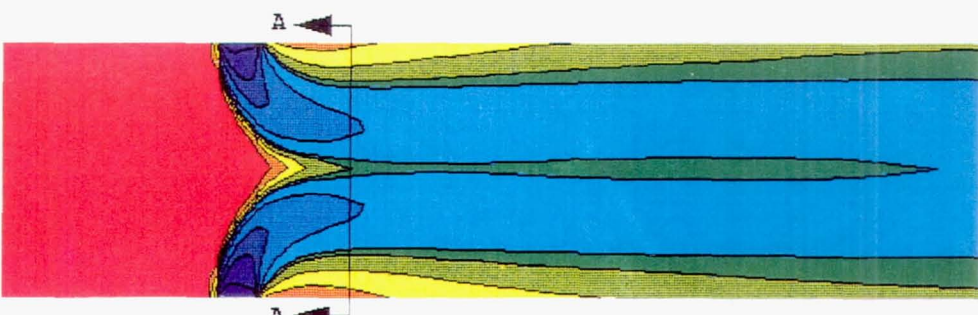
2.0

$S/H=0.375$



0.50

$S/H=0.275$



0.25

$S/H=0.25$

Plane A-A
@ $x/H=0.50$

Figure 7. Effect of Jet-to-Mainstream Mass Flow Variation on Jet Penetration at Optimum S/H: $J=36$, $L/W=4$

Axial Cross-Sections @ $x/H=0.50$

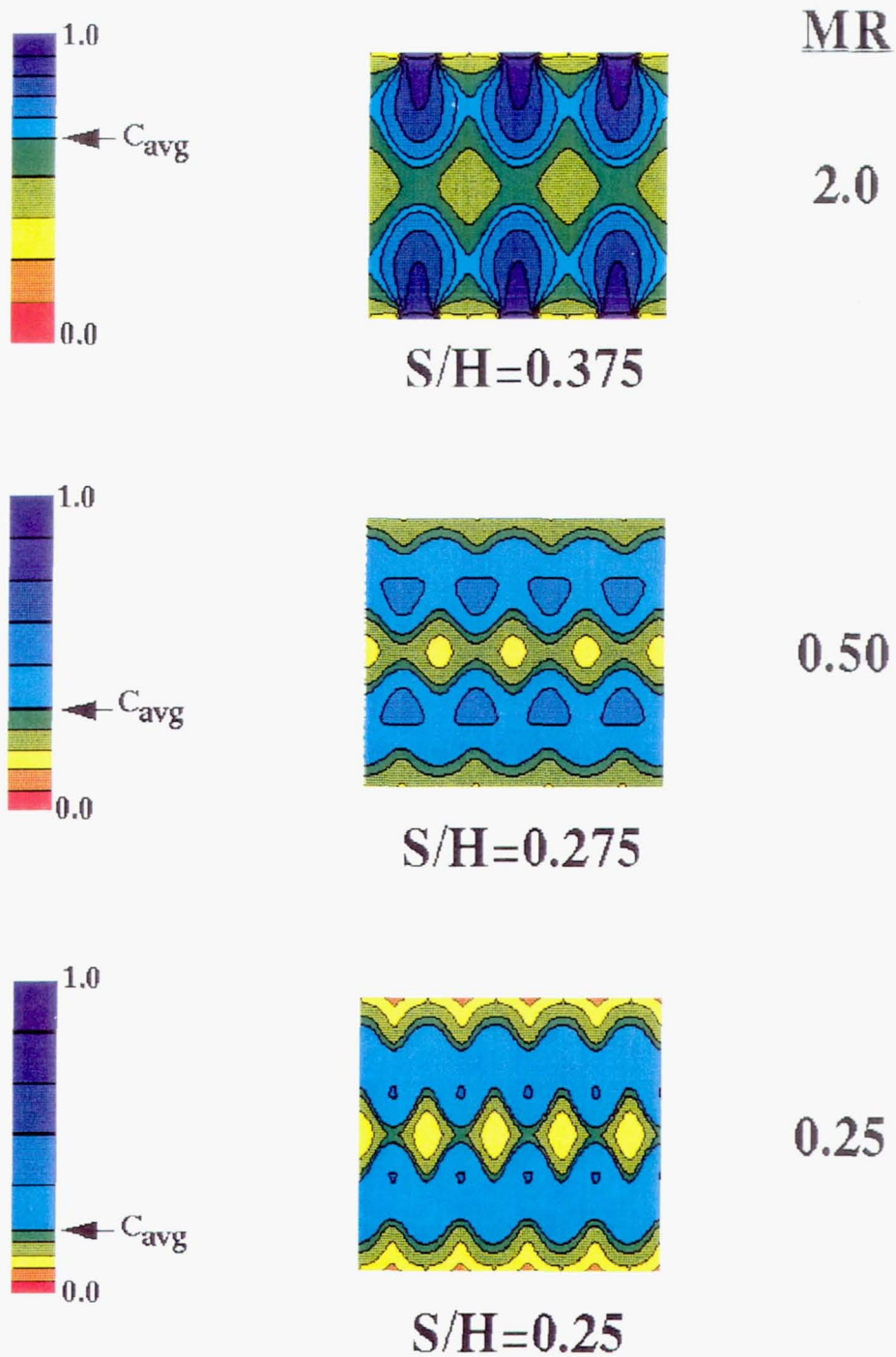


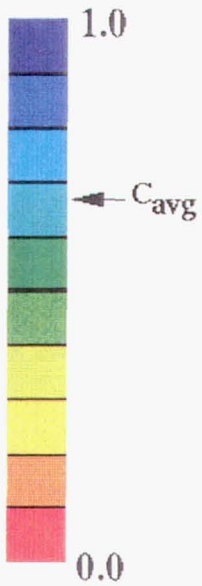
Figure 8. Effect of Jet-to-Mainstream Mass Flow Ratio on Jet Penetration: $MR=2.0$, $J=36$

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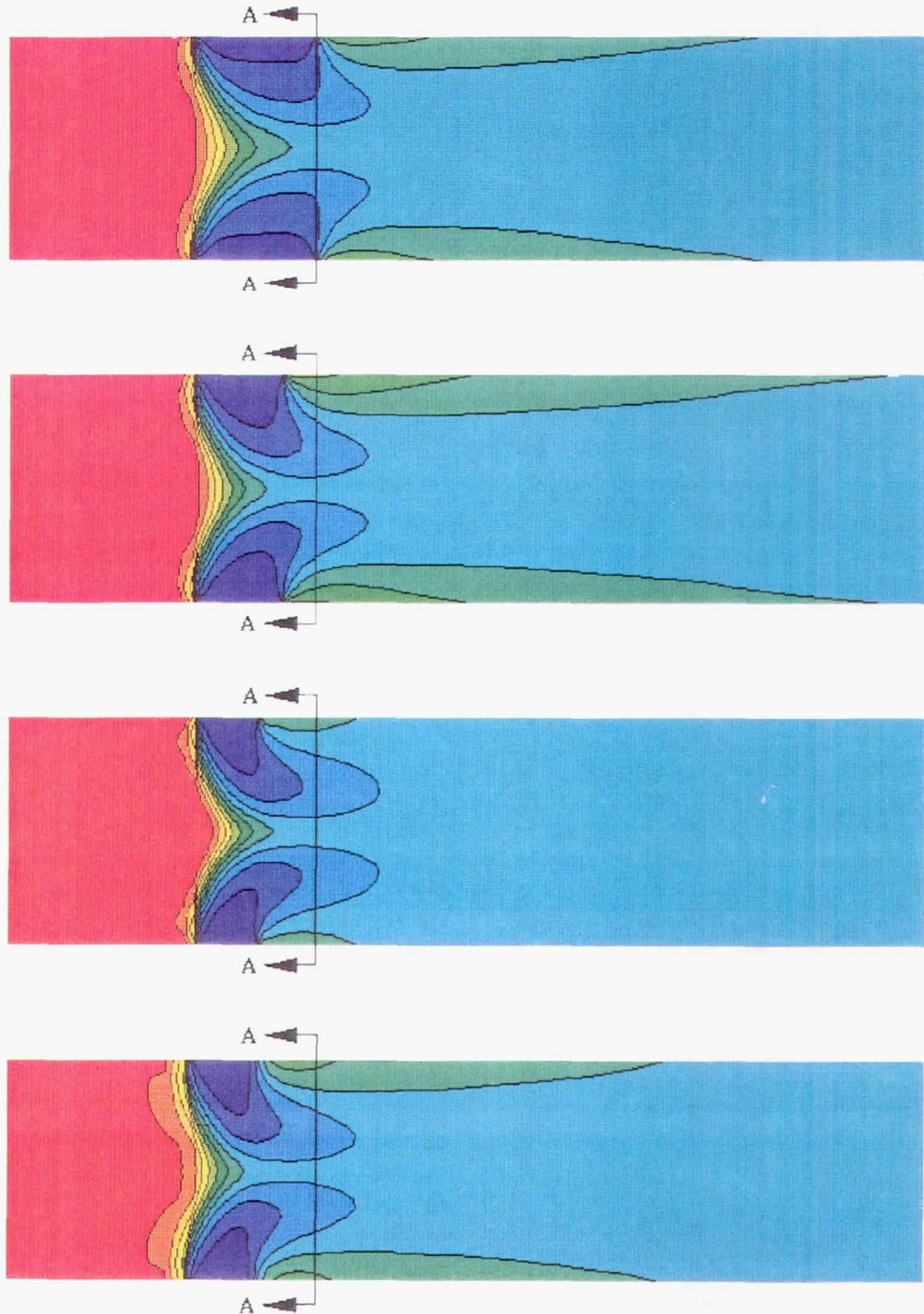
Slot Centerline @ $S/H=0.425$

L/W

Jet
Mass
Fraction



Plane A-A
@ $x/H=0.50$



4

2

1

Circle

Figure 9. Effect of Aspect Ratio on Jet Penetration: $MR=2.0$, $J=36$

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Top Injection Plane @ $S/H=0.425$

L/W

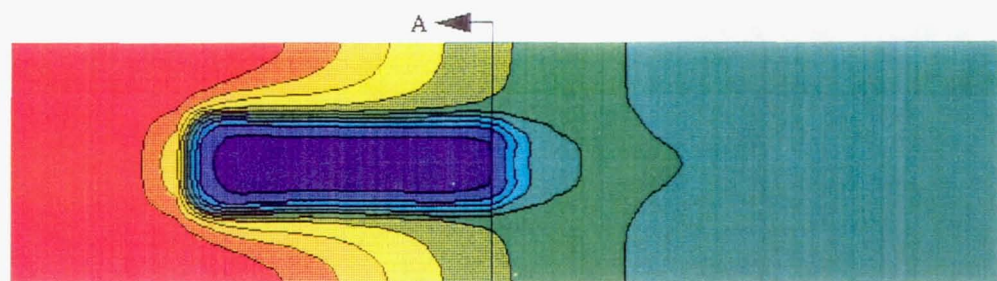
Jet
Mass
Fraction

1.0

C_{avg}

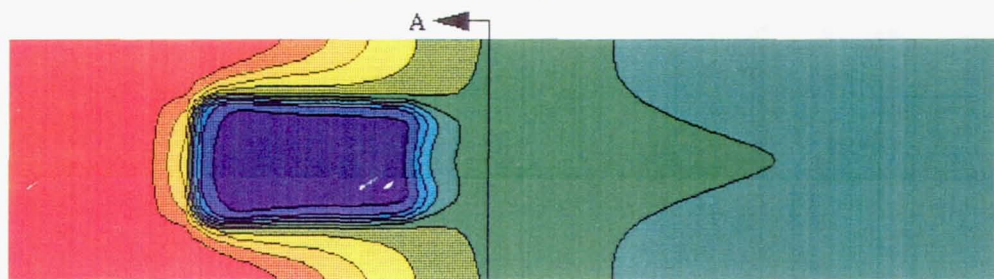
0.0

Plane A-A
@ $x/H=0.50$



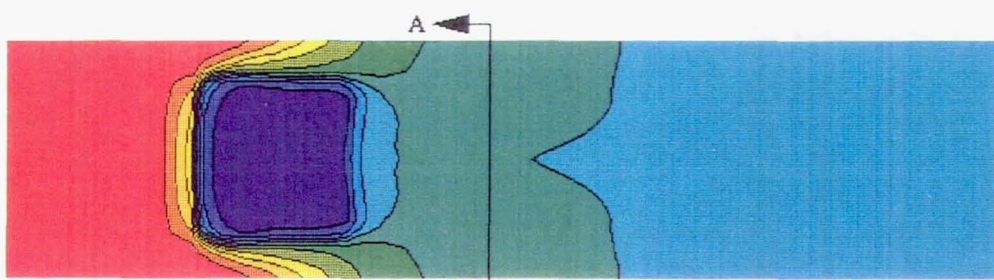
4

Jet Blockage 31%



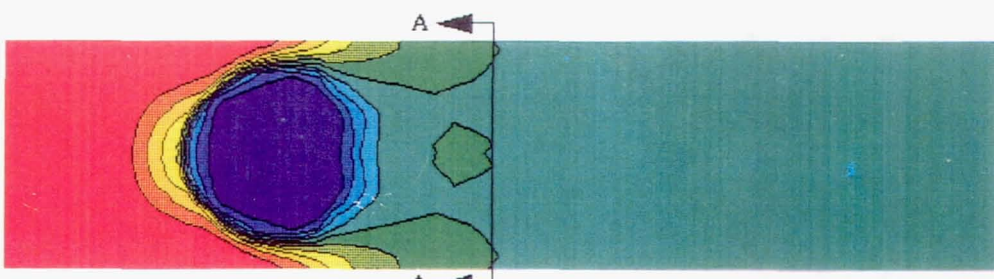
2

Jet Blockage 44%



1

Jet Blockage 63%



Circle

Jet Blockage 71%

Figure 10. Effect of Aspect Ratio on Flow Characteristics at Top Wall: $MR=2.0$, $J=36$

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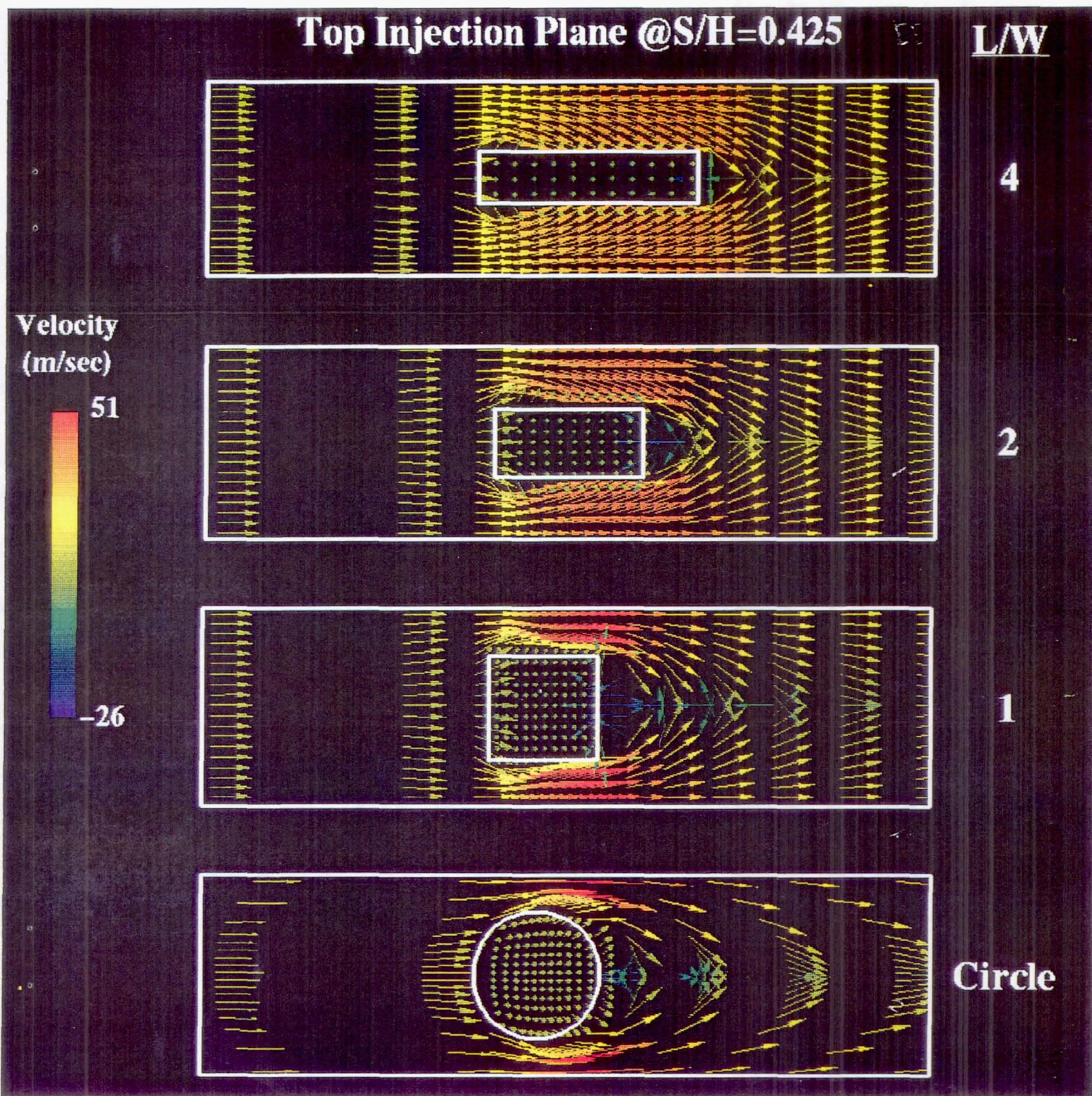


Figure 11. Effect of Aspect Ratio on Jet Wakes: $MR=2.0$, $J=36$ (Every 2nd Vector Shown)

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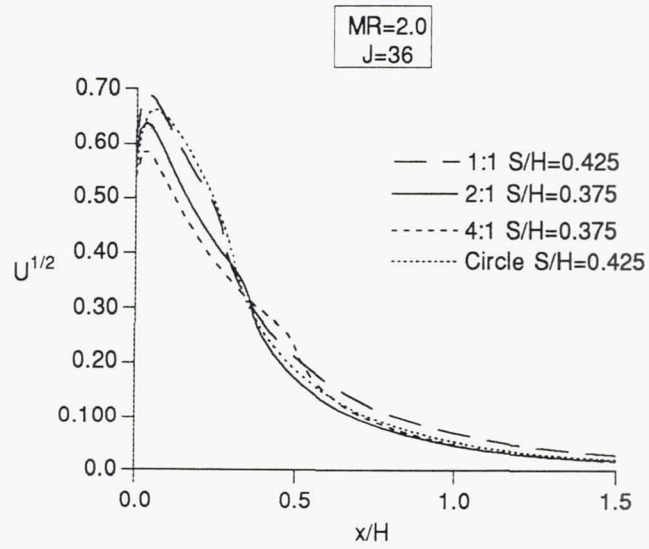


Figure 12. Effect of Aspect Ratio on Unmixedness

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Axial Cross-Sections @ $x/H=0.50$

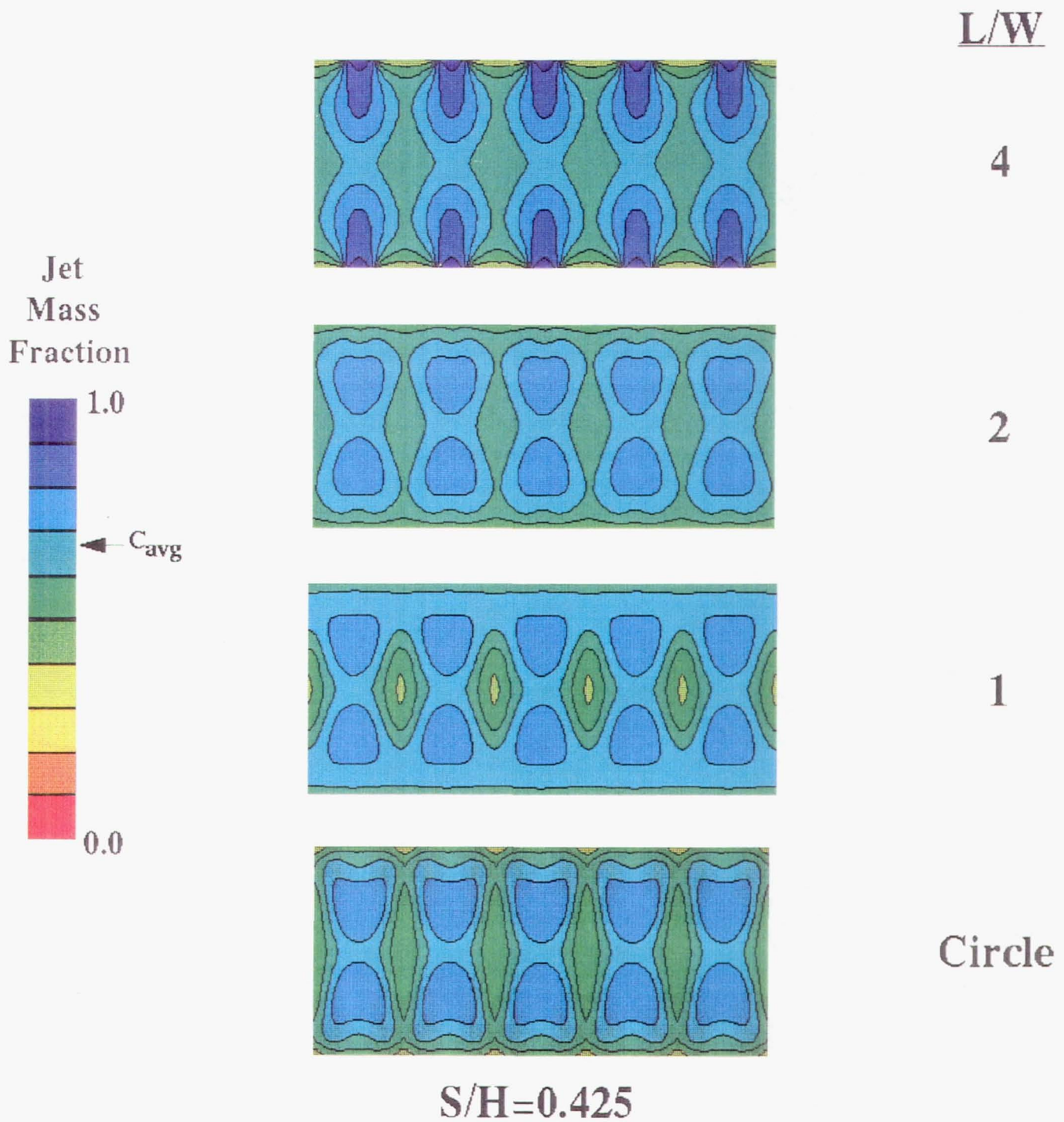


Figure 13. Effect of Aspect Ratio on Jet Penetration: MR=2.0, J=36

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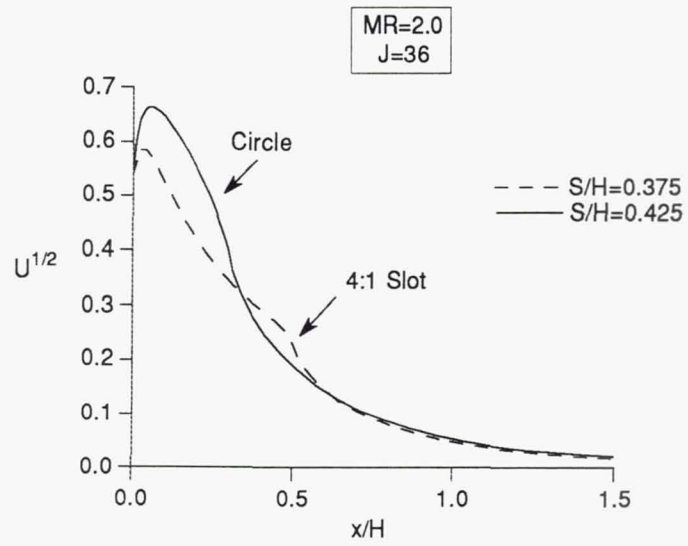


Figure 14. Unmixedness Comparison of 4:1 Slot and Circle at Optimum S/H

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13. ABSTRACT (Maximum 200 words) Isothermal CFD analysis was performed on axially opposed rows of jets mixing with crossflow in a rectangular duct. Laterally, the jets' centerlines were aligned with each other on the top and bottom walls. The focus of this study was to characterize the effects of orifice aspect ratio and jet-to-mainstream mass flow ratio on jet penetration and mixing. Orifice aspect ratios (L/W) of 4-to-1, 2-to-1, and 1-to-1, along with circular holes, were parametrically analyzed. Likewise, jet-to-mainstream mass flow ratios (MR) of 2.0, 0.5, and 0.25 were systematically investigated. The jet-to-mainstream momentum-flux ratio (J) was maintained at 36 for all cases, and the orifice spacing-to-duct height (S/H) was varied until optimum mixing was attained for each configuration. The numerical results showed that orifice aspect ratio (and likewise orifice blockage) had little effect on jet penetration and mixing. Based on mixing characteristics alone, the 4-to-1 slot was comparable to the circular orifice. The 4-to-1 slot has a smaller jet wake which may be advantageous for reducing emissions. However, the axial length of a 4-to-1 slot may be prohibitively long for practical application, especially for MR of 2.0. The jet-to-mainstream mass flow ratio had a more significant effect on jet penetration and mixing. For a 4-to-1 aspect ratio orifice, the design correlating parameter for optimum mixing $[C = (S/H)\sqrt{J}]$ varied from 2.25 for a mass flow ratio of 2.0 to 1.5 for a mass flow ratio of 0.25.				
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